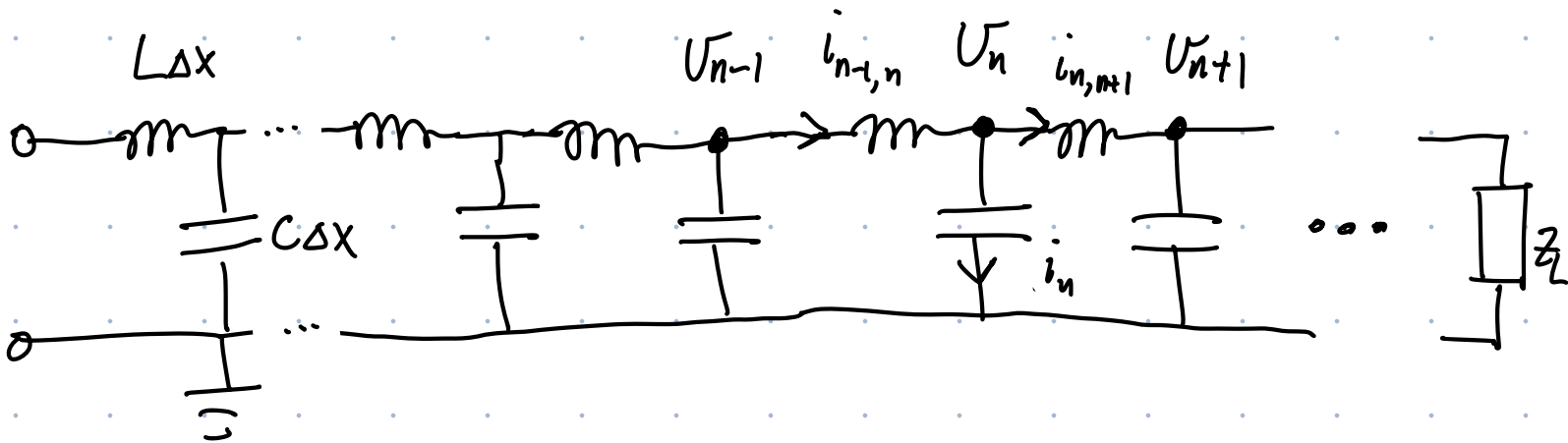


Transmission Line analysis

Sept. 11, 2025

following an analogy to a linear array of masses connected by springs.

Jake Bobowski



Junction rule at V_n :

$$\dot{i}_{n-1,n} = \dot{i}_n + \dot{i}_{n,n+1}$$

$$\therefore \dot{i}_n = \dot{i}_{n-1,n} - \dot{i}_{n,n+1}$$

$$\therefore \dot{q}_n = \dot{i}_{n-1,n} - \dot{i}_{n,n+1}$$

$$\therefore \ddot{q}_n = \frac{d\dot{i}_{n-1,n}}{dt} - \frac{d\dot{i}_{n,n+1}}{dt} \quad (1)$$

Charge on cap.

$$q_n = C \Delta x V_n$$

$$\therefore \dot{i}_n = \dot{q}_n$$

Next, if we go from U_{n-1} to U_n through the inductance, we require:

For current i_- : $\Delta U_{L-} = U_n - U_{n-1} = -L \Delta x \frac{d i_{n,n}}{dt}$

$$\therefore \frac{d i_{n,n}}{dt} = - \left(\frac{U_n - U_{n-1}}{L \Delta x} \right) = \frac{q_{n-1} - q_n}{LC \Delta x^2} \quad (2)$$

Likewise, for current i_+ :

$$\Delta U_{L+} = U_{n+1} - U_n = -L \Delta x \frac{d i_{n,n+1}}{dt}$$

$$\therefore \frac{d i_{n,n+1}}{dt} = \frac{q_n - q_{n+1}}{LC \Delta x^2} \quad (3)$$

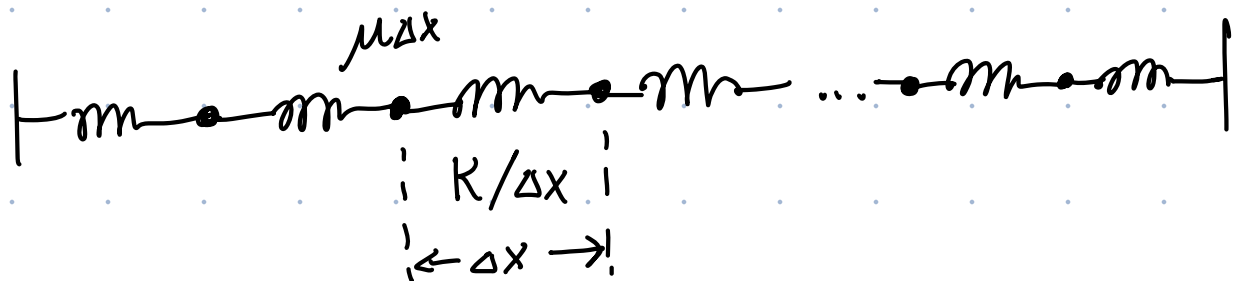
Sub (2) & (3) into (1)

$$\ddot{q}_n = \frac{q_{n-1} - q_n}{LC \Delta x^2} - \frac{q_n - q_{n+1}}{LC \Delta x^2}$$

$$\therefore LC \Delta x^2 \ddot{q}_n = q_{n-1} - 2q_n + q_{n+1}$$

(a)

Before continuing, let's make an analogy to a mechanical system $\rightarrow$ a linear array of pt. masses connected by springs.



Here, μ per unit length mass ($m = \mu \Delta x$).

The stiffness, on the other hand, must scale as $\frac{1}{\Delta x}$.

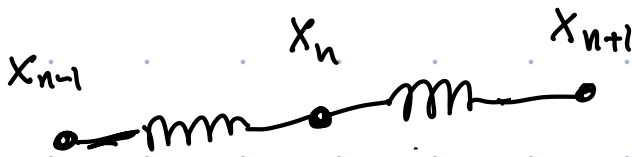
Why? Springs in series combine s.t. their stiffnesses add in inverse.



$$\frac{1}{k_{eq}} = \frac{1}{k_1} + \frac{1}{k_2}$$

$\therefore$ As we decrease Δx , we are combining more and more springs in series. To keep the overall stiffness of the system constant, we must compensate by scaling $k = \frac{K}{\Delta x}$

FBD of a single pt. mass.



$$\begin{aligned} \mu \Delta x \ddot{x}_n &= -\frac{K}{\Delta x} (x_n - x_{n-1}) + \frac{K}{\Delta x} (x_{n+1} - x_n) \\ &= \frac{K}{\Delta x} (x_{n-1} - 2x_n + x_{n+1}) \end{aligned}$$

$$\therefore \frac{\mu}{K} \Delta x^2 \ddot{x}_n = x_{n-1} - 2x_n + x_{n+1}$$

(5)

Notice that (a) and (b) have identical forms!

The TL model is analogous to the mass-spring system which itself can be used to model the physics of a 1-D lattice in which there are couplings between adjacent lattice points.

To complete the analogy, note that

$$V_L = L \frac{di}{dt} = L \frac{d^2 q}{dt^2} \quad \text{and} \quad F = m \frac{dv}{dt} = m \frac{d^2 x}{dt^2}$$

$$\therefore L \leftrightarrow m$$

L is inertia for i , like m is inertia for v .

$$V_C = \frac{q}{C} \quad \text{and} \quad F_S = kx$$

$$\frac{1}{C} \leftrightarrow k$$

$\frac{1}{C}$ couples adjacent inductors

Mass-spring system: When all springs in equil, all masses at rest (no K.E.). When a mass is displaced (x_n out of equil), the springs apply a net force to restore equil. ($\dot{x}_n \neq 0$)

LC Transmission line: When all caps at equil. charge, voltage diff. across L is zero $\& \dot{q}_n = 0$. When a cap is out of equil, it absorbs or releases charge s.t. $\dot{q}_n \neq 0$ and we get charging currents through the inductors.

Back to (a):

$$\therefore LC \Delta x^2 \ddot{q}_n = q_{n-1} - 2q_n + q_{n+1} \quad (a)$$

Consider the Taylor expansion of $f(x)$ about $x=a$:

$$f(x) \approx f(a) + (x-a)f'(a) + \frac{1}{2}(x-a)^2 f''(a) + \dots$$

Now, consider $f(x+h)$ and expand about x
Define $u = x+h$. Then, $x = u-h$

$$f(u) \approx f(\underbrace{u-h}_x) + (\cancel{u} - (\cancel{u-h})) \underbrace{f'(u-h)}_x + \frac{1}{2} (\cancel{u} - (\cancel{u-h}))^2 \underbrace{f''(u-h)}_x + \dots$$

$$\therefore f(x+h) \approx f(x) + h f'(x) + \frac{1}{2} h^2 f''(x) + \dots$$

Likewise,

$$f(x-h) \approx f(x) - h f'(x) + \frac{1}{2} h^2 f''(x) + \dots$$

$$\therefore f(x-h) + f(x+h) \approx 2f(x) + h^2 f''(x).$$

$$\therefore f''(x) \approx \frac{f(x-h) - 2f(x) + f(x+h)}{h^2}$$

In ②, we identify $q_n = q(x)$

$$\left. \begin{aligned} q_{n-1} &= q(x-\Delta x) \\ q_{n+1} &= q(x+\Delta x) \end{aligned} \right\} \Delta x \text{ is the segment length/lattice constant.}$$

$$\therefore \frac{q_{n-1} - 2q_n + q_{n+1}}{\Delta x^2} \approx \frac{\partial^2 q(x)}{\partial x^2}$$

The equality becomes exact in the continuum limit $\Delta x \rightarrow 0$, and $q_n \rightarrow q(x)$.

$$\therefore \textcircled{a} \text{ becomes } LC \ddot{q}(x) \approx \frac{\partial^2 q(x)}{\partial x^2}$$

$q(x)$ is the capacitor voltage. $\therefore$ the voltage across the parallel TL conductors is $V = \frac{q}{C}$

$$\therefore \frac{\ddot{q}(x)}{C} \rightarrow \ddot{V}(x) \quad \frac{\partial^2 q(x)/C}{\partial x^2} \rightarrow \frac{\partial^2 V(x)}{\partial x^2}$$

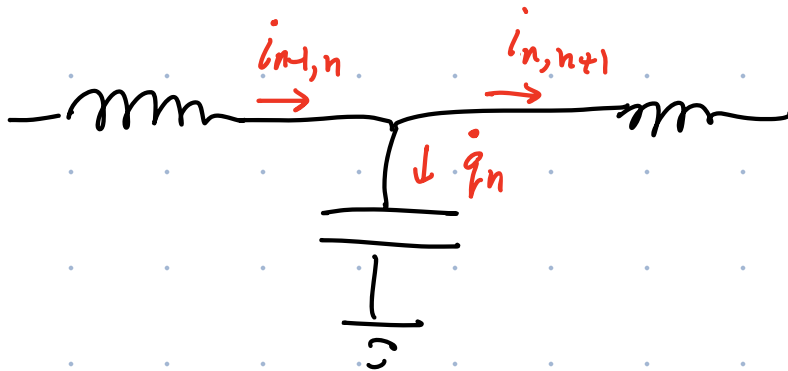
We have recovered the first wave equation

$$\boxed{\frac{\partial^2 V}{\partial x^2} = LC \frac{\partial^2 V}{\partial t^2}} \quad \textcircled{4}$$

To get the 2nd wave equation, return to $\textcircled{3}$:

$$\frac{di_{n+1}}{dt} = \frac{q_n - q_{n+1}}{LC \Delta x^2}$$

$$\therefore LC \frac{d^2 \dot{i}_{n,n+1}}{dt^2} = \frac{\dot{q}_n - \dot{q}_{n+1}}{\Delta x^2}$$



$$\dot{i}_{n-1,n} = \dot{q}_n + \dot{i}_{n,n+1}$$

$$\therefore \dot{q}_n = \dot{i}_{n-1,n} - \dot{i}_{n,n+1}$$

$$\dot{q}_{n+1} = \dot{i}_{n,n+1} - \dot{i}_{n+1,n+2}$$

$$\therefore \frac{\dot{q}_n - \dot{q}_{n+1}}{\Delta x^2} = \frac{\dot{i}_{n-1,n} - \dot{i}_{n,n+1} - (\dot{i}_{n,n+1} - \dot{i}_{n+1,n+2})}{\Delta x^2}$$

$$= \frac{\dot{i}_{n-1,n} - 2\dot{i}_{n,n+1} + \dot{i}_{n+1,n+2}}{\Delta x^2}$$

$$= \frac{\partial^2 \dot{i}(x)}{\partial x^2} \text{ in the } \Delta x \rightarrow 0 \text{ limit.}$$

$$\therefore \boxed{\frac{\partial^2 \dot{i}}{\partial x^2} = LC \frac{\partial^2 \dot{i}}{\partial t^2}}$$

We've now recovered (5) the wave equations we found in class. The rest of the analysis proceeds as presented in the class notes.

Let's return to the analogous mass-spring system and show how the discrete TL-like analysis leads to phonon dispersion relations found in solid-state physics (PHYS 474).

$$\therefore \frac{\mu}{K} \Delta x^2 \ddot{X}_n = X_{n-1} - 2X_n + X_{n+1}$$

(6)

$$\mu \Delta x \rightarrow m$$

$$\frac{\Delta x}{K} \rightarrow K$$

$$\therefore m \ddot{X}_n = K (X_{n-1} - 2X_n + X_{n+1})$$

$$\text{Assume } X_n \approx A e^{j(\omega t - k n a)}$$

where I've take $\Delta x = a$ to be the lattice const of the linear chain.

$$\ddot{X}_n = -\omega^2 X_n$$

~~XXXXXXXXXXXXXXXXXXXX~~

Note:

$K \rightarrow$ spring const.

$$k \rightarrow \frac{2\pi}{\lambda}$$

$$\therefore -m\omega^2 \cancel{Ae^{j\omega t}} \cancel{e^{-jka}} = K \left[\cancel{Ae^{j\omega t}} \cancel{e^{-jka}} e^{jka} - 2 \cancel{Ae^{j\omega t}} \cancel{e^{-jka}} + \cancel{Ae^{j\omega t}} \cancel{e^{-jka}} e^{-jka} \right]$$

$$\therefore -m\omega^2 = K \left[\underbrace{e^{jka} + e^{-jka}}_{2\cos ka} - 2 \right]$$

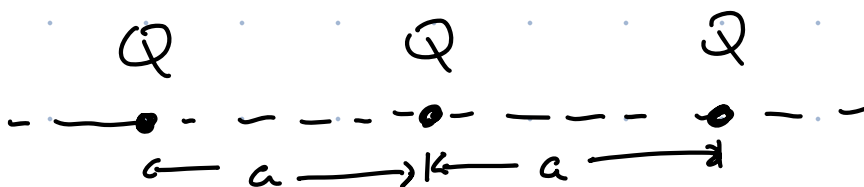
$$-m\omega^2 = -2K \left[1 - \cos ka \right]$$

usually, use the identity $\sin^2 \frac{\theta}{2} = \frac{1 - \cos \theta}{2}$

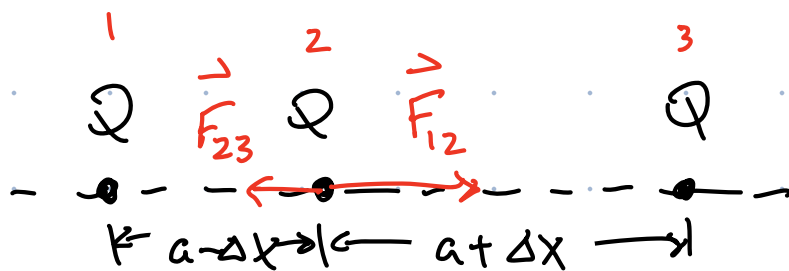
$$\therefore \omega^2 = 4 \frac{K}{m} \sin^2 \left(\frac{ka}{2} \right) \quad (6)$$

This is the phonon (lattice vibration) dispersion relation.

Why is K the right model? Consider an array of 3 ions of charge Q in a lattice.



In equil., the force on the middle charge due to its neighbours is zero. Now, displace centre charge by $\Delta x \ll a$.



Force in opp-
dir'n of
displacement Δx .
i.e. restoring force

The net force on 2 is

$$- \left[\frac{k_e Q^2}{(a - \Delta x)^2} - \frac{k_e Q^2}{(a + \Delta x)^2} \right]$$

$$= - \frac{k_e Q^2}{a^2} \left[\underbrace{\left(1 - \frac{\Delta x}{a}\right)^{-2}}_{\approx 1 + 2\frac{\Delta x}{a}} - \underbrace{\left(1 + \frac{\Delta x}{a}\right)^{-2}}_{\approx 1 - 2\frac{\Delta x}{a}} \right]$$

$$\approx - \frac{k_e Q^2}{a^2} \left(\frac{4\Delta x}{a} \right) = - \left(\frac{4k_e Q^2}{a^3} \right) \Delta x$$

Of the form $F_s = -K \Delta x$

$$\omega / \quad K = \frac{4k_e Q^2}{a^3}$$

Return to ⑥.

$$\omega^2 = 4 \frac{K}{m} \sin^2\left(\frac{ka}{2}\right)$$

Consider the case in which $\lambda \gg a$. In this case, the long wavelength phonons don't resolve the discrete structure of the lattice. It, instead, sees a continuous string.

$$\text{when } \lambda \gg a, \quad ka = \frac{2\pi a}{\lambda} \ll 1$$

$$\text{and } \sin^2\left(\frac{ka}{2}\right) \approx \left(\frac{ka}{2}\right)^2$$

$$\therefore \omega^2 = \frac{4K}{m} \frac{(ka)^2}{4} = \frac{K}{m} \left(\frac{2\pi}{\lambda}\right)^2 a^2$$

$$= \frac{(Ka)}{(m/a)} \left(\frac{2\pi}{\lambda}\right)^2$$

$\frac{m}{a} = \mu$ the linear mass density

$Ka = T$ the tension in the string.

$$(\cancel{2\pi}f)^2 = \frac{T}{\mu} \left(\frac{\cancel{2\pi}}{\lambda} \right)^2$$

$$\lambda f = c = \sqrt{\frac{T}{\mu}}$$

, where c is the speed of wave on the stretched string. Increasing the tension on the string increases the wave speed.